

## Cross Reference to Related Applications

This application is a continuation of International Patent Application No. PCT/EP0/15127, filed December 20, 2001, designating the United States of America, and published in German as WO 02/051579, the eatire disclosure of which is incorporated herein by reference. Priority is claimed based on Federal Republic of Germany patent application no. DE 100 64 327.2, filed December 22, 2000, and based on Federal Republic of Germany patent application no. DE 100 64 325.6, filed December 22, 2000.

## Background and Summary of Invention

The investion relates to a process gas for use in laser machining processes, such as laser welding or laser beam fusion cutting. The invention further relates to a process for laser machining materials, whereby a focused laser beam impiges against the surface of the work piece to be machined, and a process gas stream is directed against the surface of the work piece.

Due to the properties of the later beam, in particular its intensity and ease of focusing, laters are used dody in many areas of material processing. The later machining systems used are known in the art. In general, these comprise a later machining head, if applicable comprising a nozale arranged coaxially to the later heam. Often, later machining systems are used in conjunction with CNC controls of golde machines for an xy-cutting direction. In addition, in later beam outning, handling systems for three-dimensional work pieces are being used with increasing frequency. An automatic adjustment of cutting parameters (later proceed adjusted to the current cutting speed during the cutting process) based upon the contour to be cut is generally a preprendictie for a good out quality, even round abort processing frequency.

Within the scope of the invention, a Souscel laser beam is understood to be a laser beam that is focused essentially on the surface of the work piece. In addition to the methods predominantly used, comprising laser beams that are Socared on the surface of the work piece, the invention can also be applied with the seldom used variant in which the beam is focused on the precisely on the surface of the work piece.

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In many laser material machining processes, metallic and/or other materials are heated to temperatures at which a reaction with the cuveloping gases occurs. Thus, in many cases industrial gases are employed in order to allow these material machining processes to be implemented more effectively, more rapidly, and/or with improved quality.

Worldwick, laser beam cutting is the most frequently employed laser metahning process. For example, in Germany more than 100 40 of laser machining systems are used for cutting. In laser beam cutting, differentiation is made between laser beam flame cutting, laser beam flushed cutting, and laser beam sublimation cutting, is laser beam flushed cutting, and the service of the cutting subject to the service of the cutting service and the point of separation using the laser beam. The metted material is forced out of the cut joint via a process gaz. Laser beam flusion cutting using a process gas under high pressure has proven effective in cutting specially seate, but is also used with other materials such as structural steels and aluminum. An inert gas is usually used as the process gas in laser beam fission cutting.

In laser beam welding, process gazes fulfill different purposes. The court of and reduction of the plasma is imperative at high laser power levels. This is known, for example, from the publication "Laser in Nebell" [Laser in the Mist], Dr. W. Danzer and Klaus Behleri, journal LASER, edition 1872, pages 12 through 36. Other objectives such as protection against conduction, metalburgical optimization, and/or a maximization of speed and quality (spatter formation, porce, seam quality) have up to now been neglected. In laser beam welding, the process of using intert shielding gazes such as belium or argon is known. Nitrogen is also usual at times. Now and then, and histories are also added in and quantities.

The speed of the welding and cutting processes with the laser beam is limited by the balance between "energy introduced – energy lost (relation, thermal conduction)". The energy of the laser beam is highly concentrated, however with materials that cannot be cut with the help of the exothermal reaction with oxygen this energy becomes the limiting parameter.

For example, in cutting a 3 mm steel sheet using a 900 w laser and pure oxygen as the process gas, in addition to the 900 watts of energy coming from the laser, an additional 600 watts from the burning of the iron in the cutting joint enter into the cutting process. This results in a cutting speed of approximately 3 m/min.

However, in cutting a 3 mm chromium-nickel steel sheet using a 900 watt laser, for example, which due to the resulting slag is not cut with oxygen, but must be cut with an inert gas such

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as nitrogen or argon, this additional energy is missing from the reaction Fe+  $\frac{1}{2}$ O<sub>2</sub>  $\rightarrow$  FeO. The maximum outting speed decreases correspondingly to approximately 1.5 m/min.

An object of the present invention is thus to reveal a process gas and a method of the type described at the beginning which will permit improved laser machining. In this, a high cutting speed for laser beam fusion cutting is sought. In particular, the goal is to enable a high-quality, process-safe, and reproducible laser beam fusion cutting process. In laser beam sedding, the goal is to achieve a maximization of speed adquilty, in addition to controlling and reducing the plasma, using the process gas specified in the invention. In this, the invention is aimed primarily at cases in which an inert gas is customatily used as the process gas.

This object is attained according to the invention with a process gas that contains at least oxygen and hydrogen, in addition to at least one inert gas.

The invention is based upon the concentration of energy from the reaction 2  $H_2 + O_2 \rightarrow 2$   $H_2O$  at the point at which the laser beam is working.

The reaction 2 H2 + O2 contributes various advantages that work well with the laser beam:

- 1. It is clean.
- It is more or less reductive depending upon the mixing ratio H<sub>2</sub>/O<sub>2</sub>.
- It is very rapid.
- 4. It is high energy.
- It will run especially in places where high temperatures are present, i.e. at the point of machining.

If the process gas specified in the invention is used with the laser beam fusion cutting process, the metal components emerge from the cutting process bright. In laser welding, the invention produces a positive effect on plasma formation.

In improvements according to certain preferred embodiments of the invention, a process gas mixture that will produce a reductive effect can be used. By selecting the hypostocishometric ratio of caygen to hydrogen in the process gas mixture with respect to the reaction  $2R_1 + O_2 \rightarrow 2R_1O_1$ , the degree of reductive effect of the process gas can be established. This means that, depending upon the selection of the hypostocichometric ratio of caygen to hydrogen in the process gas mixture can be used. Thus, in laser

machining a valuable opportunity for adjusting to conditions present in individual cases, including those of the material to be processed, is provided. In laser fusion cutting, the reductive effects of the process gas cause the metal components to emerge from the cutting process bright.

Advantageously, the inert gas in the process gas can contain one or more of the gas components from the group nitrogen, argon, and helium. However, nitrogen is preferably used as the inert gas in laser fusion cutting.

According to certain preferred embodiments of the invention, the process gas can contain a share of oxygen of between 0.1 and 30 % by volume, preferably between 0.5 and 25 % by volume, most preferably between 1 and 20 % by volume.

Advantageously, the share of hydrogen in the process gas amounts to between 1 and 70 % by volume, preferably between 5 and 60 % by volume, most preferably between 10 and 50 % by volume.

In a further development of certain preferred embodiments of the invention, the process gas is mixed from a gas mixture containing at least hydrogen or hydrogen and inert gas (in particular nitrogen and/or argon) and air.

Advantageously, according to certain preferred embodiments of the invention, the process gas used in later beam fusion cutting is comprised largely of nitrogen and argon. In particular, the cutting gas and contain more than 10% by volume nitrogen and/or argon, referably between 20 and 98 % by volume nitrogen and/or argon, most preferably between 30 and 95 % by volume nitrogen and/or argon. It is also possible for other gases besides nitrogen and argon to be contained in the inert gas quantities listed.

In certain preferred embodiments of the invention, the process gas used in laser beam fusion cutting can be comprised of

- a ternary mixture of nitrogen, oxygen, and hydrogen,
- a ternary mixture of argon, oxygen, and hydrogen,
- a quaternary mixture of nitrogen, argon, oxygen, and hydrogen.

Solve appears for larger machining work pieces specified in the invention

In embodiments of the process for laser machining work pieces specified in the invention, such as laser beam fusion cutting or laser beam welding, a process gas as disclosed above is used.

In certain preferred embodiments of the invention, by establishing the resits of oxygen to hydrogen in the process gas with respect to the reaction  $2 \, H_1 + O_2 \rightarrow 2 \, H_2 O_1$ , the degree of reductive effect produced by the process gas can be determined. This means that based upon the selection of the hypostoichiometric ratio of oxygen to hydrogen in the process gas, a more or less reductive process gas can be used. In this manner, the process gas can be adjusted to meet existing conditions.

The process gas can be supplied premixed to the laser machining system.

In an alternative embodiment of the invention, at least individual components of the process gas mixture are mixed in the laser welding/cutting machine before tracking the welding/putting mozzle, and/or are swited in the welding/cutting mozzle. In this case, the welding/cutting machine or the welding/cutting mozzle contains correspondingly designed devices, in anticulte built-in components and two yukies.

The process gas specified in certain preferred embodiments of the invention is suited for use in laser beam flission cetting, and the process is suited for the laser beam flusion cetting of materials that cannot be cut via a laser beam flame cutting process. The invention allows high-quality, reproducible cutting at an increased cutting speed via laser fusion, and has proven to be process-safe. Further, the invention results in an improvement in the formation of conferentions in later beam fusion cutting.

The process gas specified in certain preferred embodiments of the invention is suited for use in laser welding, and the process is suited for the laser welding of coated materials, above all steels, in particular galvanized steels. Tests on galvanized steel sheets produced very positive results. To some extent, the speed can be greatly increased.

As a rule, the invention necessitates no modifications to existing laser devices and armatures.

The invention can be used in conjunction with all types of lasers. In certain preferred embodiments of the invention, it is suited for use in laser machining using Nd-YAG lasers, diode lasers, and CO<sub>2</sub> lasers. OO 9:

With laser beam fusion cutting as an example, with the help of the energy balance, it can be demonstrated how much additional energy can be supplied to the laser cutting process with the help of the invention.

The following gas quantities are used in certain preferred embodiments of the invention:

- 6 m<sup>3</sup>/h mixture of 50% H<sub>2</sub>/N<sub>2</sub> and 5 m<sup>3</sup>/h compressed air.
  Resulting mixture at point of cutting:
  - 11 m<sup>3</sup>/h with approximately 10% O<sub>2</sub>, 30% H<sub>2</sub>, and 60% N<sub>2</sub>.

In the combustion of the 10% O<sub>2</sub> in this mixture, 255,000 kJ are released per hour, which translates to an additional output of 70 kW. If only I/100 of this power is used in the cutting joint, this means that the overall power of the laser cutting process is nearly doubled.

The foregoing description and examples have been set forth merely to illustrate the invention and are not intended to be limiting. Since modifications of the described embodiments incorporating the spirit and substance of the invention may occur to persons skilled in the art, the invention should be constructed broadly to include all variations within the scope of the seconded claims and equivalent thereon.